

LAMS-2801

CIC-14 REPORT COLLECTION  
**REPRODUCTION  
COPY**

**C.9**

**LOS ALAMOS SCIENTIFIC LABORATORY  
OF THE UNIVERSITY OF CALIFORNIA ○ LOS ALAMOS NEW MEXICO**

---

A CODE FOR REDUCING MANY-GROUP  
CROSS SECTIONS TO FEW GROUPS



## LEGAL NOTICE

This report was prepared as an account of Government sponsored work. Neither the United States, nor the Commission, nor any person acting on behalf of the Commission:

A. Makes any warranty or representation, expressed or implied, with respect to the accuracy, completeness, or usefulness of the information contained in this report, or that the use of any information, apparatus, method, or process disclosed in this report may not infringe privately owned rights; or

B. Assumes any liabilities with respect to the use of, or for damages resulting from the use of any information, apparatus, method, or process disclosed in this report.

As used in the above, "person acting on behalf of the Commission" includes any employee or contractor of the Commission, or employee of such contractor, to the extent that such employee or contractor of the Commission, or employee of such contractor prepares, disseminates, or provides access to, any information pursuant to his employment or contract with the Commission, or his employment with such contractor.

Printed in USA. Price \$ 1.25. Available from the  
Office of Technical Services  
U. S. Department of Commerce  
Washington 25, D. C.

LAMS-2801  
UC-32, MATHEMATICS AND  
COMPUTERS  
TID-4500 (18th Ed.)

**LOS ALAMOS SCIENTIFIC LABORATORY**  
**OF THE UNIVERSITY OF CALIFORNIA    LOS ALAMOS    NEW MEXICO**

---

**REPORT WRITTEN:** December 1962

**REPORT DISTRIBUTED:** February 11, 1963

**A CODE FOR REDUCING MANY-GROUP  
CROSS SECTIONS TO FEW GROUPS\***

by

Ralph S. Cooper

\*This report supersedes LAMS-2747.

Contract W-7405-ENG. 36 with the U. S. Atomic Energy Commission

All LAMS reports are informal documents, usually prepared for a special purpose and primarily prepared for use within the Laboratory rather than for general distribution. This report has not been edited, reviewed, or verified for accuracy. All LAMS reports express the views of the authors as of the time they were written and do not necessarily reflect the opinions of the Los Alamos Scientific Laboratory or the final opinion of the authors on the subject.





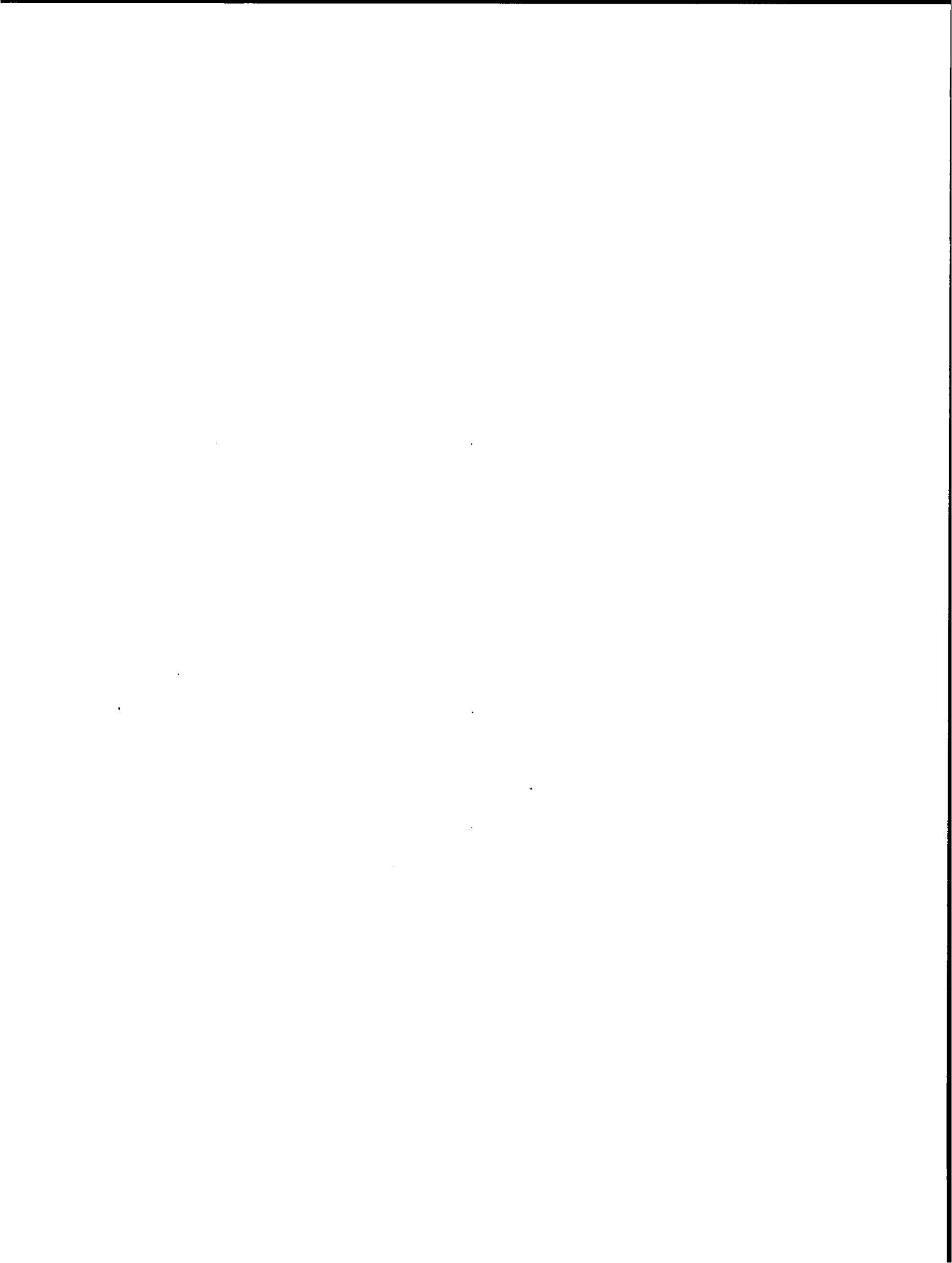
## ABSTRACT

A code (ZOT) has been written which will produce few-group neutron cross sections from many-group sets based on a given flux spectrum or one computed for an infinite medium. The cross-section format is that of  $S_n$  transport theory including the possibility of upscattering in energy. The code is written in the Floco II system for use on the IBM 704 or IBM 7090.



CONTENTS

	Page
Abstract . . . . .	3
Introduction . . . . .	7
Cross Section Input . . . . .	8
The Equations for Group Collapsing . . . . .	10
General Description of the Code . . . . .	13
Code Details . . . . .	14
Input . . . . .	14
Output . . . . .	18
Operation . . . . .	19
Operation on IBM 7090 . . . . .	20
Results . . . . .	20
Appendices . . . . .	23
I Example . . . . .	23
II ZOT Code Listings and Flow Diagrams . . . . .	27





## INTRODUCTION

While many-group cross sections are necessary for computing a large variety of problems with a single set of cross section parameters, it is often desirable to reduce the number of groups used for particular problems. Multidimensional  $S_n$  and diffusion codes are becoming available but are time-consuming with many energy groups. Where many  $S_n$  one-dimensional problems must be run for parameter studies, for temperature or perturbation effects, or when coupled to hydrodynamic codes, specially tailored few-group cross sections would be advantageous.

George Bell has suggested (internal memo, July 3, 1958) recipes for collapsing many-group parameters assuming a many-group flux spectrum. This can be obtained from a single many-group calculation for the system or approximated, for example by solving the infinite medium (space independent) equations.

A code (ZOT) has been written which will collapse groups according to a given flux spectrum or using a self-generated infinite medium flux. Code details and the results of several test cases are given.

## CROSS SECTION INPUT

The code is designed for the standard Los Alamos  $S_n$  transport cross section format. For each energy group (denoted by subscript or superscript  $g$  and running from  $g = 1$  for the highest energy to  $G$  for the lowest) the neutron cross sections are entered in the following order:

$\sigma_{ac1}$ $\sigma_{ac2}$ $\cdot$ $\cdot$ $\sigma_{aci}$	}	optional activity (ac) $\sigma$ 's, e.g., $\sigma_{n,p}$
$\nu\sigma_f$		$\nu$ (neutrons/fission) times the fission cross section
$\sigma_{tr}$		the transport cross section (occasionally labeled $\sigma_g$ )
$\cdot$ $\cdot$ $\cdot$ $\sigma_{g+2,g}$ $\sigma_{g+1,g}$	}	upscattering from groups of lower energy (higher $g$ indices) to the group $g$
$\sigma_{gg}$		scattering within the group
$\sigma_{g-1,g}$ $\sigma_{g-2,g}$ $\cdot$ $\cdot$ $\cdot$	}	downscattering from groups of higher energy to the group $g$

The activity  $\sigma$ 's are not used in the solution of the transport equation, but are available for calculation of activities from the results of criticality calculations. The most commonly appearing one is  $\sigma_a$  (absorption).<sup>\*</sup> In the solution of the transport equation the absorption is accounted for implicitly in the transport cross section  $\sigma_{tr}$ , which includes  $\sigma_a$ . Note that through error or intent, the absorption used by the transport code may be different from that which may appear as one of the activity  $\sigma$ 's. We shall always deal with the  $\sigma_a$  derived from the transport and scattering  $\sigma$ 's:

$$\sigma_a^g = \sigma_{tr}^g - \sum_{\text{all } g'} \sigma_{g',g} \quad (1)$$

where all  $g'$  includes  $g' = g$ . The number of activity  $\sigma$ 's and up- and downscattering for each group will be given implicitly by noting the position in the table of  $\sigma_{tr}$ ,  $\sigma_{gg}$ , and the last  $\sigma_{g',g}$ . If these are called  $h_t$ ,  $h_s$ , and  $h_d$  respectively, then:

$$\text{number of activity } \sigma \text{'s} = h_t - 2$$

$$\text{number of upscattering } \sigma \text{'s} = h_s - h_t - 1$$

$$\text{number of downscattering } \sigma \text{'s} = h_d = h_s.$$

---

<sup>\*</sup>This one is required by the Los Alamos DTK transport code.

The ZOT code will take the many-group cross sections for elements or mixtures and reduce the number of groups to  $K(K \leq G)$  by combining some of the groups according to equations given later. The new groups must have energy limits which are a subset of the many-group limits. We shall use  $k$  to denote the few-group energy index (and  $i$  for the  $\sigma$  position, analogous to  $h$  for the many-group set). Thus each group  $k$  will be composed of one or more of the groups  $g$  of the input  $\sigma$ 's. For example, the first of the few-group set ( $k = 1$ ) might be composed of  $g = 1, 2,$  and  $3$  of the input many-group set. Our equations will use a simple summation sign to indicate a summation over all  $g$  in a particular  $k$  group.

#### THE EQUATIONS FOR GROUP COLLAPSING

Fission spectrum (fraction of fission neutrons out in each energy group)

$$\chi_k = \sum_{g \text{ in } k} \chi_g \equiv \sum \chi_g \quad (2)$$

Activity and fission cross sections are weighted linearly by the flux  $\phi$

$$\sigma_{ac}^k = \frac{\sum \phi_g \sigma_{ac}^g}{\sum \phi_g} \quad (3)$$

Transport cross section

$$\sigma_{tr}^k \equiv \sigma_k = \frac{\sum \varphi_g}{\sum \varphi_g / \sigma_g} \quad (4)$$

or

$$\sigma_k = \sum \varphi_g \sigma_g / \sum \varphi_g \quad (5)$$

Both options (inverse and linear averaging) are available.

Transfer cross sections from group  $k'$  to group  $k$

$$\sigma_{k',k} = \frac{\sum_{\substack{g' \text{ in } k' \\ \text{and} \\ g \text{ in } k}} \varphi_{g'} \sigma_{g',g}}{\sum_{g' \text{ in } k'} \varphi_{g'}} \quad (6)$$

For the many-group set, absorption cross sections ( $\sigma_a$ 's) are found from Eq. (1) and are collapsed with linear averaging

$$\sigma_a^k = \sum \varphi_g \sigma_a^g / \sum \varphi_g \quad (7)$$

These are sufficient to define the new set. The elastic scattering  $\sigma_{kk}$  is determined from the other few-group constants by

$$\sigma_{kk} = \sigma_k - \left( \sum_{k' \neq k} \sigma_{k,k'} \right) - \sigma_a^k \quad (8)$$

For conciseness in annotating the code, we define

$$\varphi_k = \sum \varphi_g \quad (9)$$

Different cross sections may be computed for each region (i.e., core and reflector) separately, but a single velocity spectrum is used for a given problem, and this must be weighted by the total fluxes in each region. The region volumes are used as a measure of the total flux.

$$v_k = \frac{\left( \sum_r v_r \sum \varphi_{g,r} \right)}{\left( \sum_r v_r \sum \varphi_{gr} / v_g \right)} \quad (10)$$

The infinite medium fluxes ( $\varphi^0$ ) can be generated by

$$(\sigma_g - \sigma_{gg})\varphi_g^0 = x_g + \sum_{g' \neq g} \sigma_{g' \rightarrow g} \varphi_{g'}^0 \quad (11)$$

These are solved successively from the highest energy group until groups with nonzero upscattering are reached, upon which the remaining equations are solved simultaneously.

## GENERAL DESCRIPTION OF THE CODE

The code is written for the Floco II assembly system\* (LAMS-2339) and is intended to be fully compatible with the Floco II assembled SNG routines. The code accepts multigroup cross sections and input data on atomic composition and computes collapsed group parameters for the mixtures described for each special region. An option allows collapsing the element microscopic cross sections separately. The code will accept flux spectra as input, will compute infinite medium fluxes, or can use the flux used in the previous spacial region (mixture) regardless of its source. The volumes can be given directly or can be computed from the coordinates for planes, infinite cylinders, or spheres. The code assumes there has been sufficient size allotted to the up- and downscattering in the output groups and will stop with an on-line comment if this is not true. The many-group set is divided into a few groups, each containing one or more of the original groups according to the wishes of the user. The input and output are printed off-line (on-line if sense switch #6 is down), and the output fission spectrum, velocities, and cross sections are punched on-line, suitable for direct inclusion in the new  $S_n$  codes. (They may be used in the Floco I version of SNG by placing nine punches in columns 3 and 21.) The code will normally average  $(\sigma_{tr})^{-1}$  but will

---

\* This will run on the IBM 704 or IBM 7090 with the appropriate Floco II assembly program. The standard deck is for the 704; modifications for 7090 operation are discussed in a later section.

average  $\sigma_{tr}$  if requested. In either case, a comment will be printed describing which was done.

## CODE DETAILS

### Input

The input is divided into two parts: the parameters which precede the code and the data which follow it.

The parameters determine the sizes of data storage blocks and are used in determining exits and loop lengths in the code. They consist of information on the size of the problem (e.g., number of mixtures), options such as the method of transport weighting, and the cross section table size. Parameters are put on Floco cards, following a "load parameters" pseudo-instruction (\*0000S00, see IAMS-2339 and example in Appendix I). There are three sets labeled P00, G00, and K00, each requiring a load parameters instruction. All are fixed point numbers. The code was designed originally to form mixture macroscopic cross sections in a manner similar to the SNG code. This requires two tables which we shall label NO and MO. The NO table contains a fixed point identification number (ID#) for each region, followed by the ID numbers of the elements in that particular region. The elements are numbered implicitly by the order in which they are input. The MO block contains the atomic densities corresponding to the elements in each region and zeros in the positions



occupied by the mixture numbers in the NO table. This is illustrated in the example (Appendix I). The lengths of the NO and MO blocks are required for input parameter P05.

One could get  $\sigma$ 's for collapsed microscopic elements with this arrangement by placing each element in a separate region with an atom density of 1.0. However, since this is a common use of the code, an alternate way to obtain these  $\sigma$ 's with simpler input has been built into the code. This is signaled by letting the mixture specification parameter P05 (or N) be zero. The number of regions R (P02) is put equal to the number of elements E, and P03 is input as 2E. There is no need for certain of the data blocks (NO, MO, FO), and only one set of weighting fluxes need be entered for all elements.

#### 1. Parameters

<u>Position</u>	<u>Symbol</u>	<u>Description</u>
P01	PID	Problem identification number.
P02	R	Number of regions (or number of elements for element calculation).
P03	M	Number of mixtures + number of elements (or twice number of elements for element calculation).
P04	W	Volume specification, described later.
P05	N	Number of mixture specifications, i.e., length of NO and MO tables (N = 0 for element calculations).
P06	T	Transport $\sigma$ averaging 0 for inverse, 1 for linear average.

Parameters, continued

<u>Position</u>	<u>Symbol</u>	<u>Description</u>
G01	G	Number of input groups.
G02	$h_t$	Position of $\sigma_{tr}$ in $\sigma$ table.
G03	$h_s$	Position of $\sigma_{gg}$ .
G04	$h_l$	Position of last $\sigma$ in a group (number of $\sigma$ 's per group).
G05	U	Number of groups with nonzero upscattering, assumed to occur in the lowest energy groups.
K01	K } $i_t$ } $i_s$ } $i_l$	Output cross section parameters (similar to input group parameters, but may have smaller values except for $i_t$ ). The equivalent of G05. $i_s$ is not needed.
K02		
K03		
K04		

W, Volume Specification

<u>W</u>	<u>Meaning</u>
0	Volumes are supplied in WO data block.
1	Planar distances of regions are supplied in WO data block; code will compute volumes $V = (r_{i+1} - r_i)$ and place them in WO data block.
2	Cylindrical radii supplied in WO; code computes $V = (r_{i+1}^2 - r_i^2)$ , etc.
3	Spherical radii supplied; $V = (r_{i+1}^3 - r_i^3)$ , etc.
4	Volumes are not supplied; velocities are computed separately for each region.

## 2. Data

The data follow the code and are on Floco cards preceded by Floco "load data" pseudo-instructions (\*0000S0). The order of the data blocks is immaterial. Binary cards (e.g., flux dumps) may be loaded behind a Floco "load data" card if they contain the data in the correct number and order. Binary card addresses will be ignored.

<u>Block</u>	<u>Description</u>	<u>Type</u>	<u>Number of Entries</u>
CO	Group separation, a table giving the largest value of g in each output group.	fixed	K
FO*	The flux source for each region 0 -- flux supplied 1 -- calculate $\infty$ medium flux 2 -- use flux from previous region.	fixed	R
F2†	The weighting fluxes for each region.	floating	GXR
NO*	The mixture specifications, similar to the SNG input. For each region there is an identifying number, followed by the labels of the elements in that region.		
MO*	The atomic densities ( $\times 10^{-24}$ ) of the elements in the order given in NO. Zeros in the positions corresponding to region numbers in NO serve to delimit the regions.	floating	N
WO	Volume or radius input.	floating	R
SO	Input fission neutron spectrum.	floating	G
VO	Input group velocities.	floating	G

---

\* Can be omitted for microscopic element calculation.

† Only one set (G entries) needed for microscopic element calculation.

<u>Block</u>	<u>Description</u>	<u>Type</u>	<u>Number of Entries</u>
PO	The input (and mixture) cross section block. The elements are numbered implicitly by the order in which they are placed in the input deck. The regions are labeled by consecutive numbers beginning with E + 1, as in the DSN code. See example (Appendix I).	floating	Input = $h_l \times G \times E$ Total = $h_l \times G \times M$

### Output

The output includes off-line (on-line if sense switch #6 is down) listing of all of the input blocks, descriptively labeled and of the mixture cross sections (in the PO block) and the mixture absorption cross sections. This is followed by a print of the output fission spectrum, velocities, absorption cross sections, and mixture cross sections.

The fission spectrum, velocities, and mixture cross sections for each region are punched in that order on separate cards (or blocks of cards), ready for direct insertion into the DSN code. Cards may also be used in the Floco I SNG code by putting nine punches in columns 3 and 19. Should trouble arise, one can obtain an input print by transferring manually to (1016)<sub>8</sub> and pressing start twice. One can obtain an on-line output print by setting sense switch #6 down and transferring manually to (1017)<sub>8</sub> and pushing start twice.

When the calculation is finished, an on-line statement to that effect will be printed. Pushing start will then result in an on-line print of the storage map giving locations of all code and data blocks.

## Operation

The present deck (10-30-62) has all necessary loading and transfer cards in it. The three parameter cards follow ZOT card number 001, and the data cards follow card number 076.\* The ZOT deck should be preceded by an on-line identification card to identify the user on the off-line listing. ZOT card 00D calls Floco II from the Los Alamos utility tape 1, and may be replaced by a Floco II card deck.

Running time --  $\leq 1$  minute per case + readin time, unless there are more than 10 upscattering groups.

Problem size -- for the 8K machine about  $(4000)_{10}$  words are available for data. The largest block will be the input and mixture cross sections (PO) which will be  $h_p \times G \times (E + R)$  numbers. Almost all problems can thus be done on an 8K 704.

Stops -- the only programmed stops are for the cases in which insufficient down- or upscattering has been allowed in the output groups. The code will print an on-line comment and stop. One can then transfer to  $(1016)_8$  to obtain an input print. There is an error stop (usually insufficient space) in the matrix solver subroutine, and three possible divide checks which are described in Appendix II.

Sense switches -- setting sense switch #6 down causes on-line printing of both input and output. An on-line print of the results can be obtained by transferring manually to  $(1017)_8$  and pushing start twice (with sense switch #6 down).

---

\* This is a change from the earlier (9-09-59) deck.

### Operation on IBM 7090

The ZOT deck (001 to 080) will work without modification on the 7090. However the appropriate Floco II assembly system must be used, and therefore the ZOT 000 card, which is an XX Floco 2 card for calling the 704 version from tape, must be replaced by the equivalent for the 7090. This is a set of two cards (2-FL2 01 and 2-FL2 02) for calling Floco from tape, or a master set of cards containing Floco for use if it is not already on the utility tape in the Los Alamos format. Note that header or identification cards follow the Floco II cards, making the deck arrangement

2-FL2 01 } 2-FL2 02 }	Floco II, call in from Los Alamos 7090 utility tape.
Header Card	* in column 1, followed by name, phone, etc.
ZOT 001	Initialize Input, etc., as in 704 version.

### RESULTS

A series of DSN transport calculations were made to investigate the accuracy of the reduced cross section sets. Few-group results are typically within 2% of the many-group results, but each new situation should be checked, especially where the spectrum changes rapidly in

space. Some typical results obtained in 1959 with  $S_4$  SNG transport calculations are listed in Table I. Further calculations are presently under way to study the extent of application and the effects of varying the group spacing, the method of averaging the transport cross section, etc. For example, a 3 group calculation of the C/U = 2400 base sphere with different group aggregations (6, 11, 1) gave only 0.4% error using fluxes generated in an 18 group DTK transport code, compared to 2.5% error with the spacing (6, 6, 6) as listed in Table I. However, the (6, 11, 1) spacing with infinite medium fluxes appears to give a larger error (7%) although this result is difficult to understand and may be in error.

Table I

Bare U<sup>235</sup> Sphere

# Groups *	Flux Source	Radius	Sign, % Error	# Iterations
6	-	8.686	-	22
2	SNG 6 group	8.732	+0.53	15
2	$\infty$ medium	8.742	+0.65	15
1	SNG 6 group	8.776	+1.03	19
1	$\infty$ medium	8.753	+0.75	16

## Bare Graphite Sphere C/U = 300

# Groups *	Flux Source	$k_{eff}$	Sign, % Error	# Iterations
18	-	0.9700	-	119
6	18 group SNG	0.9634	-0.7	127
6	$\infty$ medium	0.9778	+0.8	126
3	18 group SNG	0.9582	-1.15	136
3	$\infty$ medium	0.9883	+1.9	122

## Bare Graphite Sphere C/U = 2400

# Groups *	Flux Source	$k_{eff}$	Sign, % Error	# Iterations
18	-	0.967	-	51
6	18 group SNG	0.934	-3.4	77
6	$\infty$ medium	0.950	-1.7	75
3	18 group SNG	0.943	-2.5	111
3	$\infty$ medium	0.984	+1.7	112

\* Each of the collapsed groups contained equal numbers (3 or 6) of groups of the 18 group set.



## Appendix I

### Example

Consider an  $H_2O$  reflected,  $H_2O$  moderated sphere, for which it is desired to reduce the Hansen-Mills 18 group cross sections to 3 groups. There are thus two regions with the following composition:

<u>Atom density <math>\times 10^{-24}</math></u>	<u>Core</u>	<u>Reflector</u>
H	0.0663	0.0668
O	0.0332	0.0334
$U^{235}$	$1.288 \times 10^{-4}$	

Assume one wishes to compute the infinite medium fluxes for the core and reflector compositions to use in weighting the 18 group cross sections and that the core and reflector radii will be supplied for weighting the velocities. The three output groups are chosen to contain 6, 9, and 3 input groups, respectively, starting from the high energy end. Parameters and data for the above problem follow on Floco coding forms and are included in the ZOT decks.



FLOCO 704

77	78	79	80	PROBLEM		
				PROGRAMMER	DATE	PAGE

C	OPERATION				ADDRESS				REMARKS	C	OPERATION				ADDRESS				REMARKS								
	P		R		S		X				R		S		P		R			S		X		R		S	
	1	2	3	4	5	6	7	8			9	1	2	3	4	5	6	7		8	9	1	2	3	4	5	6
0	9	*							S	0																	
1	10										1	10															
2	19										2	19															
3	28										3	28															
4	37										4	37															
5	46										5	46															
6	55										6	55															
7	64										7	64															
0	9	*							V	0																	
1	10										1	10															
2	19										2	19															
3	28										3	28															
4	37										4	37															
5	46										5	46															
6	55										6	55															
7	64										7	64															
0	9	*							P	0																	
1	10										1	10															
2	19										2	19															
3	28										3	28															
4	37										4	37															
5	46										5	46															
6	55										6	55															
7	64										7	64															
0											0																
1	10										1	10															
2	19										2	19															
3	28										3	28															
4	37										4	37															
5	46										5	46															
6	55										6	55															
7	64										7	64															



## Appendix II

### ZOT Code Listings and Flow Diagrams

The coding is relatively simple and straightforward except perhaps where the transfer cross sections  $\sigma_{g'g}$  are involved. Flow diagrams are given for those cases and for the master or flow code. Annotated listings are given for all code blocks, as well as summaries of the data and code blocks.

#### Summary of Data and Code Blocks

##### Data

A0 (A1)	Input absorption cross sections by region.
A2 (A3)	Output absorption cross sections by region.
C0	Separation of output groups.
F0	Flux source table.
F2 (F3)	Many-group flux by region.
F4 (F5)	Few-group flux by region.
G0	Table of the output group corresponding to each input group.
M0	Atomic density table.
M1 (M2)	Matrix for flux with upscattering.
NO	Mixture composition table.

Data (contd.)

P0 (P1, P2) Many-group cross sections by element and mixture.  
Q0 (Q1, Q2) Output cross sections by mixture.  
V0 Many-group velocities.  
V1 Few-group velocities average over volume.  
V2 (V3) Few-group velocities for each region.  
W0 Volume or radius table.

Code

801 Flow code (master code).  
803 Data assignment.  
804 Form mixture  $\sigma$ 's.  
805 Calculate many-group fluxes,  $\phi_g$ .  
806 Set region addresses.  
807 Calculate many-group absorption  $\sigma_a^g$ .  
810 Calculate transfer cross sections  $\sigma_{k'k}$ .  
811 Collapse cross sections  $\sigma_{ac}$ ,  $v\sigma_f$ ,  $\sigma_{tr}$ ,  $\sigma_a$ .  
812 Calculate few-group self-scattering  $\sigma_{kk}$ .  
813 Generate code constants.  
814 Calculate fission spectrum  $X_k$ .  
815 Calculate velocities.  
816 Input print.  
817 Output print and punch.

Code (contd.)

822 Place element  $\sigma$ 's in region blocks.  
823 Set flux for element calculation.  
843 - 867 and 871 Print remarks and headings.  
870 Matrix solver subroutine IA-S885.

Use of Temporary Storage Block T00

T01-T07 Temporary use only.  
T10  $\sigma_t^g$  region base address and region index in decrement.  
T11  $\phi_g$  region base address.  
T12  $\sigma_t^k$  region base address.  
T13  $\phi_k$  region base address.  
T14  $v_k$  region base address.  
T15  $\sigma_a$  region base address.  
T16  $\sigma_a$  region base address.  
T17 Not used.  
T20  $h_l - h_s$   
T21 # elements  
T22  $h_s - h_t - 1$   
T23  $h_s - h_t$   
T24  $h_t + 1$   
T25  $i_t + 1$

### Error Stops

Location

<u>Octal</u>	<u>Region</u>	<u>Symbolic</u>	<u>Type</u>	<u>Cause</u>
5314	805	X47	divide check	$\sigma_g - \sigma_{gg} = 0$ . Not allowed in calculating flux.
5427	805	Y62	halt	Matrix error. Stop, check size.
5461	805	Z14	divide check	$\varphi_k = \sum \varphi_g = 0$ . Check flux input.
5617	810	X46	halt	Too few upscattering cross sections allowed in output (on-line print).
5674	810	X53	halt	Too few downscattering cross sections allowed in output (on-line print).
6304	815	X50	divide check	$\sum V_r v_k^r = 0$ . Check volume and velocity inputs.

### ZOT Deck

XX Floco 2

or

ZOT 000

Floco II tape calling card.

ZOT 001

Initialize, allow space for parameters.

Input

Parameters P00, G00, K00 cards.

ZOT 002

Assigns temporary storage T00, 30<sub>8</sub> spaces.

003

Assigns formula space 100<sub>8</sub> for 801, 1500<sub>8</sub> for 804, 50<sub>8</sub> for 803, and 420<sub>8</sub> for 870.

004 to 025

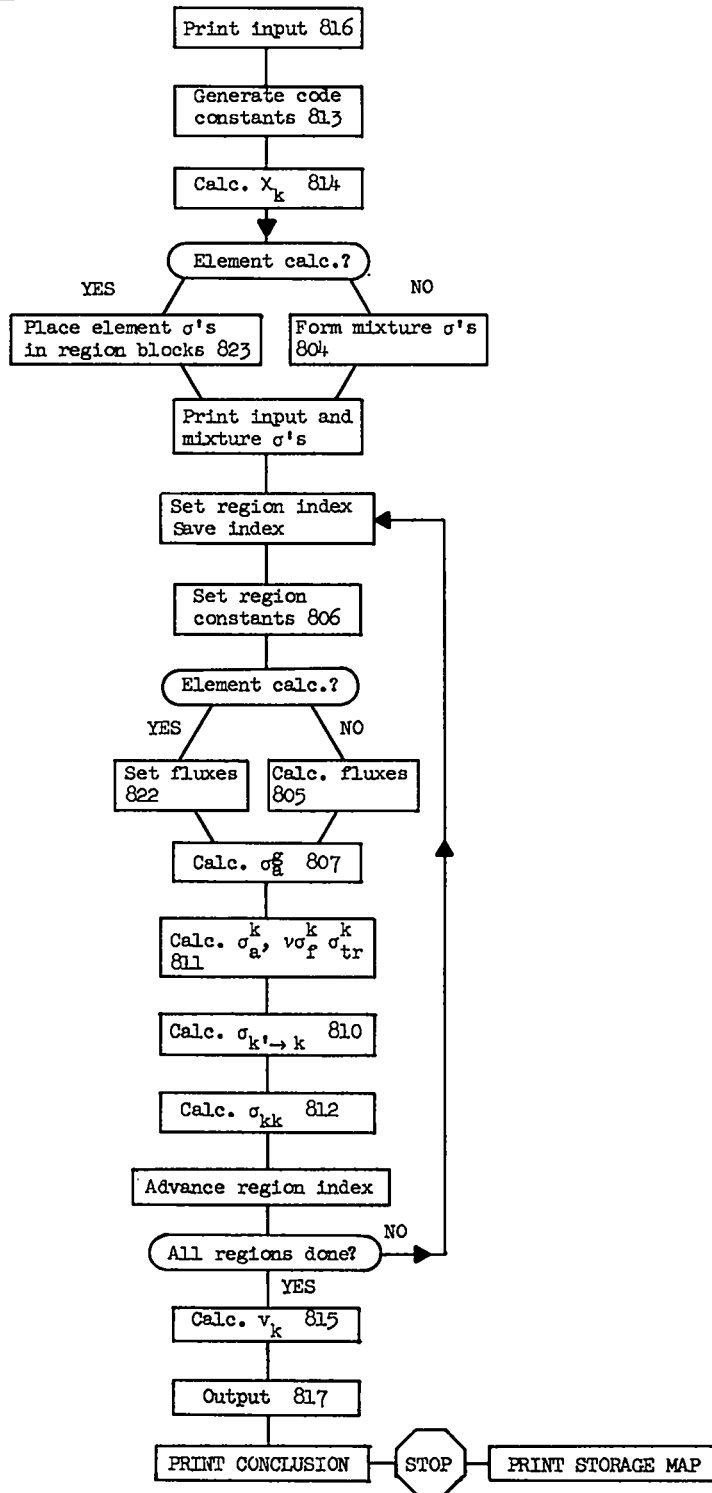
Remarks for printing headings.



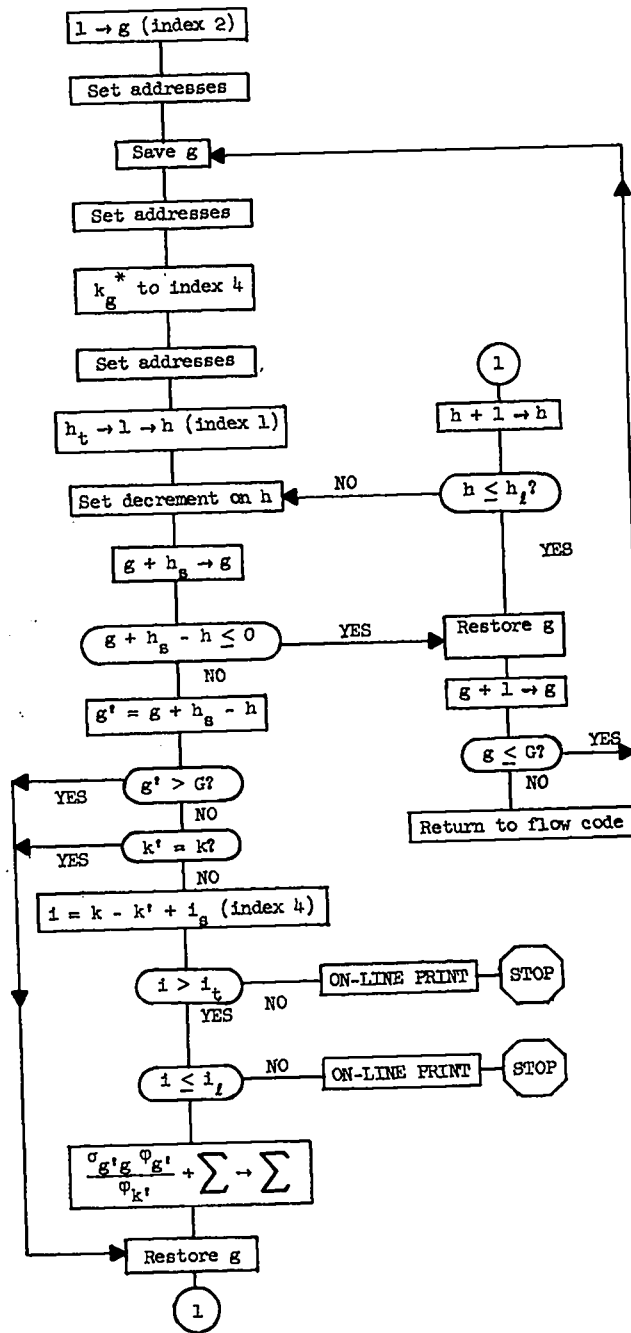
ZOT Deck, continued

026	Load data assign code (803).
027, 028	Data assign code (symbolic binary).
029	Execute data assign code.
030	Load matrix solver (870).
031 - 041	Matrix solver (binary).
042	Load formulas 804 to 823.
043 - 073	Formulas in symbolic binary.
074	Load flow code 801.
75, 76	Flow code.
Input	Data.
77	Transfer to flow code.
78, 79	Blank.

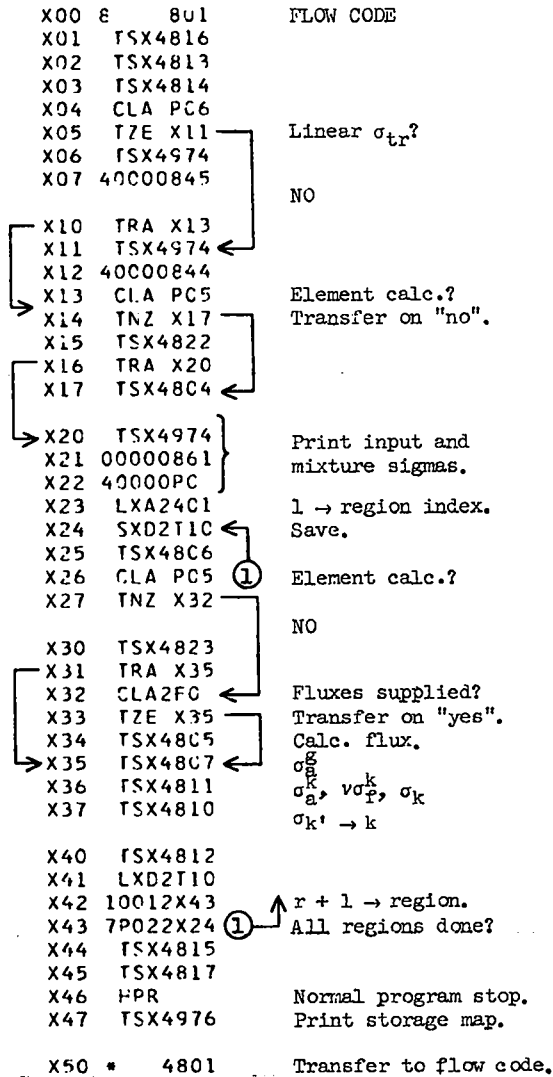
801 FLOW CODE







\* $k_g$  is the output group corresponding to an input group  $g$ .



X00	8	AC4	FORM MIXTURE $\sigma$ 's
X01	LXA14C1		$1 \rightarrow i$
X02	CLA1NC		$N_i$
X03	STA IC1		Save $N_i$ . ②
X04	CLA1MC		$M_i$ atom density.
X05	TN2 X14	}	$N_i \rightarrow j$
X06	LXA2T01		
X07	CLA PC*		
X10	SUB2P2		
X11	STA X26	}	Set address for region sigmas.
X12	STA X27		
X13	TRA X31		
X14	STC IC2		$N_i \rightarrow$ index.
X15	LXA4TC1	}	Set address.
X16	CLA P0*		
X17	SUB4P2		
X20	STA X24	}	Put $h_j \times G$ in index.
X21	LXA2402		
X22	CLA2P2		
X23	PAX2		
X24	LDC20CC		①
X25	FMP T02		Form $M_i \times \sigma$ .
X26	FAD20CC		
X27	STO20CC		
X30	20012X24	①	Advance i.
X31	10011X32	②	
X32	7P051X02		
X33	LXD4457		
X34	TRA4001		

X00 8 8C5  
 X01 SUB 4C1  
 X02 TNZ Z21  
 X03 CLA T11  
 X04 STA X42  
 X05 STA X50  
 X06 CLA GC1  
 X07 SUB GC5

CALCULATE FLUXES  
 Use flux from previous region?  
 YES  
 NO, calc. flux.

X10 ALS 022  
 X11 STD X52  
 X12 LXA14C1  
 X13 CLA T10  
 X14 SUB1P1  
 X15 STA X37  
 X16 SUB GC2  
 X17 STA X23

# of groups with only downscattering =  $G_d$ .  
 $g = 1$   
 $\sigma_r$  base. ←  
 $\sigma_r(g)$  base. ②  
 $\sigma_g$

X20 ACD GC2  
 X21 SUB GC3  
 X22 STA X24  
 X23 CLA OCC  
 X24 FSB OCC  
 X25 STO TC3  
 X26 CLA1S0  
 X27 STO T02

$\sigma_{gg}$   
 $\sigma_g - \sigma_{gg}$   
 $x_g$

X30 SXD1TC1  
 X31 LXD2TC1  
 X32 20012X34  
 X33 TRA X46  
 X34 LXA4GC3  
 X35 1C014X36  
 X36 3G044X46  
 X37 CLA40CC

$g \rightarrow$  index 2.  
 $g' = g - 1$   
 $g' = 0$   
 $h_s \rightarrow h$   
 $h + 1 \rightarrow h$  ←  
 $h > h_s?$   
 NO,  $\sigma_{g'} \rightarrow g$  ①

X40 TZE X46  
 X41 LRS 043  
 X42 FMP2CC0  
 X43 FAD T02  
 X44 STO T02  
 X45 20012X35  
 X46 CLA TC2  
 X47 FCH TC3

$\sigma_{g'} \rightarrow g = 0?$   
 NO  
 $\Phi_{g'} \sigma_{g',g}$   
 $\sum \Phi_{g'} \sigma_{g',g}$   
 $g' = 1 \rightarrow g', g' = 0?$  ①  
 $\sum \Phi_{g'} \sigma_{g',g} / \sigma_g - \sigma_{gg}$

X50 STQ1000  
 X51 10011X52  
 X52 70C01X13  
 X53 CLA G05  
 X54 TZE Z01  
 X55 CLA T11  
 X56 STA Y35  
 X57 STA Y77

$\Phi_{g+1} \rightarrow g$   
 $g < G_d?$  NO ②  
 Upscattering present?  
 YES  
 Set up matrix solution.

X60 STZ T04  
 X61 LXD1T04  
 X62 1C011X63  
 X63 CLA M1\*  
 X64 SUB1M2  
 X65 STA Y10  
 X66 STA Y23  
 X67 STA Y24

$j = 0$   
 Save j. ← ① from Y14  
 $j + 1 \rightarrow j$   
 Set addresses on j. ②  
 from Y32

X70	SUB GC5	
X71	SUB 4C1	
X72	STA Y12	
X73	STA Y36	
X74	STA Y37	
X75	SXD1T04	
X76	LXD2T04	$j \rightarrow \text{index } 2.$
X77	10002YCO	$g = j + G_d$
Y00	SXD2T05	Save $g.$
Y01	3G012Z32	$g > G?$ Exit of matrix set.
Y02	CLA TIC	NO
Y03	SUB2P1	
Y04	STA Y07	
Y05	STA Y15	
Y06	LXA4GC2	$h = h_{tr}$
Y07	CLA4CC0	-
Y10	ST01C00	$\sigma_g \rightarrow M_{jj}$
Y11	CLA2SC	
Y12	STO GCO	$X_g \rightarrow M_{n+1,j}$
Y13	1CC14Y14	$h + 1 \rightarrow h$
Y14	3G044X61	$h > h_g?$ (1) YES
Y15	CLA40C0	NO
Y16	STO IC1	$\sigma_{g'} \rightarrow g$
Y17	SXD4Y21	
Y20	1GC31Y21	Index $i = j + h_s$
Y21	6C001Y27	$i = j + h_s - h$
Y22	TRA Z34	Patch.
Y23	FAD10C0	$-\sigma_{g'} g + M_{ij} \rightarrow M_{ij}$
Y24	ST010CC	
Y25	LXD1T04	Restore $j.$
Y26	TRA Y13	
Y27	LXD2TC5	$g \rightarrow \text{index } 2.$
Y30	SXD4Y32	
Y31	1GC32Y32	$g + h_s$
Y32	6CC02X61	$g + h_s - h = g' < 0?$ (2)
Y33	LXD1TC4	NO, restore $j.$
Y34	LFQ IC1	
Y35	FMP2CC0	
Y36	FAD 000	
Y37	STO GCO	$\Phi_{g'}: \sigma_{g'} \rightarrow g + M_{n+1,j} \rightarrow M_{n+1,j}$
Y40	TRA Y13	
Y41	ARS 001	From Z33
Y42	STD Y57	
Y43	ARS C21	
Y44	CHS	
Y45	ADD M1*	
Y46	STA Y64	
Y47	LXA1401	
Y50	LXD2M2*	
Y51	CLA1M1	
Y52	LFQ2M1	(1)
Y53	ST02M1	
Y54	STQ1M1	
Y55	20012Y56	Store matrix to agree with subroutine input requirements.
Y56	10011Y57	



```

Y57 70C01Y51 ①
Y60 LXD1457
Y61 JSX4870 ..... Matrix solver.
Y62 OHPR ..... Error stop.
Y63 OG05 001
Y64 4000 CCC
Y65 9GC52Y63
Y66 SXD1457
Y67 CLA Y64 .....

Y70 CHS
Y71 ADD G05
Y72 STA Y76
Y73 LXA1G05
Y74 LXD2X52 .....
Y75 10012Y76
Y76 CLA1000
Y77 STD2CC0 ..... Store upscattering φ
                          in regular φ block.

Z00 2C011Y75
Z01 CLA I11 ..... Normalize φ.
Z02 STA ZC7
Z03 STA Z13
Z04 STA Z15
Z05 CLM
Z06 LXA1G01
Z07 FAD1CC0 ..... G → index 1.
                          φG + ∑G-1 φG → ∑ φG
                          ∑1G φG = ∑
                          φG/∑

Z10 20011Z07
Z11 STO IC1
Z12 LXA1G01
Z13 CLA1CC0
Z14 FDH I01 .....
Z15 STQ1CC0
Z16 20011Z13
Z17 LXD4457

Z20 TRA4CC1 ..... Return to flow code
Z21 CLA I11 ..... from X02.
Z22 STA Z27 ..... Use flux from previous region.
Z23 ADD G01
Z24 STA Z26
Z25 LXA2G01
Z26 CLA20C0 ..... φG,r-1 → φG,r
Z27 STD2000




Z30 20C12Z26
Z31 TRA Z17
Z32 CLA M2* ..... From matrix set.
Z33 TRA Y41
Z34 3G051Y25 ..... i > # upscattering groups?
Z35 CLS I01 ..... NO, -σGig
Z36 TRA Y23 ..... Return to code.
Z37 80002X11 ..... Patch.



Z40 STD X77
Z41 TRA X12
Z42 H0002X60 ..... Patch.
Z43 CLA M2*
Z44 STA X64
Z45 TRA X61

```

X00	H	8C6	SET REGION ADDRESSES
X01	LXD2	T10	$r \rightarrow$ index 2.
X02	CLA	F2*	$\sigma_g$ base address.
X03	SUB2	F3	
X04	STA	T11	$\phi_{gr}$ base address.
X05	PXD2		
X06	PCX4		
X07	1T214	X10	$r + E \rightarrow$ index 4.
X10	CLA	P0*	$\sigma_g$ base address.
X11	SUB4	P2	$\sigma_{rg}$ base address.
X12	STA	T10	
X13	CLA	F4*	$\phi_k$
X14	SUB2	F5	
X15	STA	T13	$\phi_{kr}$
X16	CLA	Q0*	$\sigma_k$
X17	SUB2	Q2	
X20	STA	T12	$\sigma_{kr}$
X21	CLA	V2*	$v_k$
X22	SUB2	V3	
X23	STA	T14	$v_k^r$
X24	CLA	A0*	$\sigma_a(g)$
X25	SUB2	A1	
X26	STA	T15	$\sigma_{ar}(g)$
X27	CLA	A2*	$\sigma_a(k)$
X30	SUB2	A3	
X31	STA	T16	$\sigma_{ar}(k)$
X32	LXD4	457	
X33	TRA	4001	
X34	80002	X04	Patch to get E in decrement.
X35	CLA	T21	
X36	ALS	O22	
X37	STD	X07	
X40	TRA	X05	

X00	8	807	CALCULATE $\sigma_a^g$
X01	CLA	T15	$\sigma_a^g$ address base.
X02	STA	X16	
X03	STA	X17	
X04	STA	X33	
X05	STA	X34	
X06	LXA	24C1	$1 \rightarrow g$
X07	SXD	2T01	Save $g$ .
-----			
X10	CLA	T10	
X11	SUB	2P1	$\sigma(g, r)$ address.
X12	STA	X31	
X13	SUB	G02	
X14	STA	X15	
X15	CLA	000	$\sigma_g^g$
X16	FAD	20C0	$+ \sigma_g^g \rightarrow \sigma_{ag}$
X17	STO	2000	
-----			
X20	LXA	1T24	$h_t + 1 \rightarrow h$
X21	SXD	1X23	$i \rightarrow \text{dec.}$
X22	1GC	32X23	$g + h_s$
X23	600Q2	X37	$g + h_s - h = g'$ ②
X24	PXD		
X25	ARS	022	
X26	SUB	G01	$g' - G$
X27	TZE	X31	$g' = G?$
-----			
X30	TPL	X35	NO, $g' \geq G?$
X31	CLS	1000	NO $\sigma_{g'}^g$
X32	TZE	X35	= 0?
X33	FAD	20C0	NO $\sigma_a - \sigma_{g'}^g \rightarrow \sigma_a$
X34	STO	20C0	
X35	1001X	X36	$h + 1 \rightarrow h$
X36	7G041X	X43	$h \leq h_f$
X37	LXD	2T01	Restore $g$ .
-----			
X40	10012X	X41	$g + 1 \rightarrow g$
X41	7G012X	X07	$g \leq G?$ ①
X42	TRA	40C1	Return to flow code.
X43	LXD	2T01	Restore $g$ .
X44	TRA	X21	②

X00	8	810	CALCULATE $\sigma_{k'} \rightarrow k$
X01	LXA2401		$l \rightarrow g$
X02	TNO X04		Test accum. overflow.
X03	TRA XC4		
X04	CLA T11		$\phi_g^r$ address.
X05	STA X63		
X06	STZ T01		
X07	STZ TC2		
X10	CLA T13		$\sigma_r^k$ address.
X11	STA X64		
X12	SXD2TC1		Save g.
X13	CLA T10		$\sigma_g^g$ address. 
X14	SLB2P1		
X15	STA X62		
X16	CLA2GC		
X17	STO TC2		
X20	LXA4T02		
X21	CLA T12		
X22	SUB4Q1		
X23	STA X71		$\sigma_{tr}^k$ address.
X24	STA X73		
X25	STA T30		
X26	LXA1T24		$h_t + 1 \rightarrow h$
X27	SXD1X31		
X30	1G032X31		$g + h_g$
X31	60002X77		$g' = g + h_s - h$
X32	3GC12X74		$g' > G?$
X33	CLA2G0		
X34	STO TC3		$k' - k$
X35	SUB IC2		
X36	TZE X74		
X37	CHS		
X40	ADD KC3		$i = k - k' + i_s$
X41	STO TC4		
X42	LXA4TC4		$i \rightarrow \text{index } 4.$
X43	3K024X47		$i > i_t?$
X44	TSX4975		Print.
X45	4C000847		Too few upscat.
X46	HTR Y02		
X47	3K044X51		$i \leq i_f$
X50	TRA X54		
X51	TSX4975		Print.
X52	40000846		Too few downscat. ...
X53	HTR YC2		
X54	CLA T04		
X55	NOP		
X56	NOP		
X57	NOP		
X60	STO TC4		
X61	LXA4T03		$k' \rightarrow \text{index } 4.$
X62	LPQ1U00	}	$\frac{\phi_{g'} \sigma_{g'} \rightarrow g}{\phi_{k'}}$
X63	FMP2000		
X64	FDH4000		
X65	STQ T07		
X66	CLA TC7		
X67	NOP		

X70	LXA4TC4	Restore i.
X71	FAD40C0	$\sum \varphi g^i \sigma g^i \rightarrow g / \varphi k^i$
X72	NCP	
X73	STO40C0	$\sigma k^i \rightarrow k$
X74	LXD2TC1	Restore g.
X75	10011X76	$h + 1 \rightarrow h$
X76	7GC41X27	$h < h_p$ 
X77	LXD2T01	Restore g.
-----		
Y00	10012YC1	$g + 1 \rightarrow g$
Y01	7GC12X12	$g > G?$ NO 
Y02	LXD4457	Return to flow code.
Y03	TRA4Q01	

X00	8	811	CALCULATE $\sigma_{ac}^k, v_{tr}^k, \sigma_{tr}^k, v_r^k, \sigma_a^k$
X01	LXA24C1		1 $\rightarrow$ g
X02	LXA1401		1 $\rightarrow$ k
X03	CLA1C0		
X04	ALS 022		
X05	STD YG7		
X06	CLA T13		Set addresses.
X07	STA X42		$\phi_r^k$
X10	STA X43		
X11	STA Y24		
X12	STA Y31		
X13	STA Y33		
X14	STA Y40		
X15	CLA T14		$v_r^k$
X16	STA X50		
X17	STA X51		
X20	CLA T15		$\sigma_{ar}^g$
X21	STA X52		
X22	CLA T16		$\sigma_{ar}^k$
X23	STA X54		
X24	STA X55		
X25	STA Y23		
X26	STA Y25		
X27	CLA T11		$\phi_r^g$
X30	STA X40		
X31	CLA T12		$\sigma_r^k$ base.
X32	SUB101		
X33	STA Y02		
X34	STA Y03		
X35	SUB K02		
X36	STA X75		
X37	STA X76		
X40	CLA20C0		$\phi_r^g$
X41	STD T01		
X42	FAD10C0		$\phi_r^k = \sum \phi_r^g$
X43	STO1000		
X44	CLA T01		
X45	FDP2VC		$\phi_g/v_g$
X46	STQ T07		
X47	CLA T07		
X50	FAD10C0		$v_k = \sum \phi_g/v_g$
X51	STO1000		
X52	LDQ2000		$\sigma_{ar}^g$
X53	FMP T01		
X54	FAD10C0		
X55	STO1000		$\sum \phi_r^g \sigma_{ar}^g$
X56	CLA T10		
X57	SUB2P1		$\sigma_r^g$ base.
X60	STA YC0		
X61	SUB GC2		
X62	STA X67		$\sigma_{tr}^g$ base.
X63	STA X72		
X64	CLA PC6		Linear $\sigma_{tr}^g$ ?
X65	YZE X71		
X66	LDQ T01		YES
X67	FMP 000		$\phi_g \sigma_{tr}^g$

X70 TRA X75  
 X71 CLA TC1  
 X72 FDP CCO  
 X73 STQ T07  
 X74 CLA T07  
 X75 FAD 000  
 X76 STO CCO  
 X77 LXA44C1

Inverse  $\sigma_{tr}$ .  
 $\varphi_g / \sigma_{tr}^g$

$$\sum \varphi_g \sigma_{tr}^g \text{ or } \sum \varphi_g / \sigma_{tr}^g$$

l → index 4, i for  $\sigma_{ac}(i)$ .

Y00 LDQ4000  
 Y01 FMP TC1  
 Y02 FAD4000  
 Y03 STO4000  
 Y04 10014Y05  
 Y05 7GC24YCO  
 Y06 10012Y07  
 Y07 70002X40

$$\sum \sigma_{tr}^{g,r}(i) \varphi_r^g$$

i + 1 → i  
 i > h<sub>t</sub> - 1  
 g + 1 → g  
 g > largest g in k?

Y10 10011Y11  
 Y11 7K011X03  
 Y12 LXA1401  
 Y13 CLA T12  
 Y14 SUB1Q1  
 Y15 STA Y37  
 Y16 STA Y41  
 Y17 SUB K02

k + 1 → k  
 k > k?  
 l → k  
 $\sigma_r^f$  base.  
 $\sigma_{tr}^{k,r}$  base.

Y20 STA Y30  
 Y21 STA Y34  
 Y22 STA Y35  
 Y23 CLA1CCC  
 Y24 FDP1G00  
 Y25 STQ1000  
 Y26 CLA P06  
 Y27 TZE Y33

$$\sigma_a^k = \frac{\sum \varphi_g \sigma_a^g}{\varphi_k}$$

Linear  $\sigma_{tr}$ ?

Y30 CLA 000  
 Y31 FDP1000  
 Y32 TRA Y35  
 Y33 CLA1CCC  
 Y34 FDP 000  
 Y35 STQ 000  
 Y36 LXA44C1  
 Y37 CLA4000

YES  $\sigma_{tr}^k = \frac{\sum \varphi_g \sigma_{tr}^g}{\varphi_k}$   
 Inverse  $\sigma_{tr} = \varphi_k / \sum \varphi_g / \sigma_{tr}^g$

Y40 FDP1000  
 Y41 STQ4000  
 Y42 10014Y43  
 Y43 7K024Y37  
 Y44 10011Y45  
 Y45 7K011Y13  
 Y46 LXD4457  
 Y47 TRA4001

l → index 4 (i).  
 $\sigma_{ac}^k(i) = \frac{\sum \varphi_g \sigma_{ac}^g(i)}{\varphi_k}$   
 i + 1 → i  
 i > h<sub>t</sub> - 1?  
 k + 1 → k  
 k > k?  
 Return to flow code.

Y50 90016YC5  
 Y51 90016Y43

Dec. - 1 → dec. of Y05.  
 Dec. - 1 → dec. of Y43.

X00	8	812	$\sigma_{kk}$ CALC.
X01	STZ	TC1	$\sigma_a^k$ address.
X02	CLA	T16	
X03	STA	X20	
X04	LXA	24C1	$i \rightarrow k$
X05	SXD	2TC1	Save k.
X06	CLA	T12	
X07	SUB	2Q1	
X10	STA	X42	
X11	SUB	K02	$\sigma_k$ address.
X12	STA	X17	
X13	ACD	K02	
X14	SUB	K03	
X15	STA	X21	$\sigma_{kk}$ address.
X16	STA	X22	
X17	CLA	000	$\sigma_k$
X20	FSB	20C0	$\sigma_k - \sigma_a$
X21	FAD	0C0	+ $\sigma_{kk}$
X22	STO	000	$\rightarrow \sigma_{kk}$
X23	LXA	1T25	$i_t + 1$
X24	LXD	2T01	Restore k.
X25	SXD	1X27	
X26	1K032X27		$k + i_s$
X27	6C002X51		$k + i_s - i = k'$
X30	3K012X47		Is $k' > K$ ?
X31	CLM		NO
X32	PXD2		
X33	SUB	TC1	
X34	TZE	X47	Is $k' = k$ ?
X35	CLA	T12	NO,
X36	SUB	2Q1	
X37	SUB	K03	
X40	STA	X44	
X41	STA	X45	
X42	CLS	1CC0	$-\sigma_{k'k}$
X43	NOP		+ $\sum$
X44	FAD	000	$\rightarrow \sigma_{ki}$
X45	STO	CC0	
X46	NOP		
X47	10011X50		$i + 1 \rightarrow i$
X50	7K041X24		$i > i_s$ ? NO (1)
X51	LXD	2TC1	YES, restore k.
X52	10012X53		$k + 1 \rightarrow k$
X53	7K012X05		$k > K$ ? NO (2)
X54	LXD	4457	YES, return to flow code.
X55	TRA	4GC1	



X00 8 813 GENERATE CODE CONSTANTS  
 X01 LXA24C1  
 X02 LXA1401  
 X03 CLA 4C1  
 X04 STO T01  
 X05 CLA1CC  
 X06 ALS 022  
 X07 STD X13

X10 CLA T01 Form a table  
 X11 STO2G0 of k corresponding  
 X12 10012X13 to each g.  
 X13 70002X11  
 X14 ADD 4C1  
 X15 10011X16  
 X16 7K011X04  
 X17 CLA G04

X20 SUB G03  
 X21 STO T20  $h_f - h_s$   
 X22 CLA P03  
 X23 SUB PC2  
 X24 STO T21  $E = M - R$   
 X25 CLA G03  
 X26 SUB G02  
 X27 STO T23  $h_s - h_t$

X30 SUB 401  
 X31 STO T22  $h_s - h_t - 1$   
 X32 CLA GC2  
 X33 ADD 401  
 X34 STO T24  $h_t + 1$   
 X35 CLA K02  
 X36 ADD 4C1  
 X37 STO T25  $i_t + 1$  812, X23

X40 TRA4001

X00 8 814 CALC.  $X_k$  (fission spectrum)  
 X01 LXA24Q1 1 → index 2.  
 X02 LXA14C1 1 → index 1.  
 X03 CLALC Group limits.  
 X04 ALS 022 ②  
 X05 STD X12  
 X06 CLA2SC  
 X07 FAD1S1 ①

$$X_k = \sum_{k \text{ in } g} X_g$$


---

X10 ST01S1  
 X11 10012X12  
 X12 70002X06 ①  
 X13 10011X14  
 X14 7K011XC3 ②  
 X15 TRA4001

X00	3	815	CALC. $v$
X01	CLA	PC4	Volume specification $W$ .
X02	SUB	4C4	
X03	TZE	X54	$W = 4$ , calc. $v$ for each region.
X04	CLA	PC4	
X05	TZE	X24	$W = 0$ volumes supplied.
X06	LXA24C1		Generate volumes, 1 $\rightarrow$ index 2.
X07	STZ	I02	
X10	LXA1P04		$n \rightarrow$ index 1 = 1 (region index).
X11	LDQ	421	1.0
X12	FMP2W0		$r_i^n$
X13	LRS	043	
X14	20011X12		
X15	STO	I01	
X16	FSB	I02	$r_i^n - r_{i-1}^n$
X17	STO2W0		
X20	CLA	I01	
X21	STO	I02	
X22	10012X23		$r_i \rightarrow r_{i-1}$ $i+1 \rightarrow i$
X23	7P022X10		
X24	LXA1K01		$K \rightarrow k$ (index 1).
X25	LXA2P02		$R \rightarrow$ index 2.
X26	STZ	I01	
X27	STZ	I02	
X30	CLA	F4*	$\phi$ base address.
X31	SUB2F5		
X32	STA	X33	
X33	LDQ1000		$\phi_r^k$
X34	FMP2W0		$\sum V_r \phi_r^k$
X35	FAD	I01	
X36	STO	I01	
X37	CLA	V2*	$v$ base.
X40	SUB2V3		
X41	STA	X42	$v_r^k$
X42	LDQ1000		
X43	FMP2W0		
X44	FAD	I02	
X45	STO	I02	
X46	20012X30		$\sum_{r=1}^r V_r v_k^r$
X47	CLA	I01	Regions done.
X50	FDH	I02	$v^k$
X51	STQ1V1		
X52	20011X25		$k-1 \rightarrow k$
X53	TRA4001		Calc. done, return to flow code.
X54	LDQ	K01	$v_k$ for each region.
X55	MPY	P02	
X56	STQ	I01	
X57	LXA1I01		$R \times K$ in index 1.
X60	CLA1F4		$\phi_k / \sum \phi_g / v_g$
X61	FDP1V2		
X62	STQ1V2		
X63	20011X60		
X64	TRA4001		Return to flow code.
X65	80002X15		Patch, LRS not reliable.
X66	STQ	I01	
X67	CLA	I01	
X70	TRA	X16	

X00	8	816	INPUT PRINT
X01	TSX4974		
X02	00000850		
X03	00000851		
X04	00000852		
X05	00061PC0		Parameters.
X06	00000853		
X07	00051G00		
-----			
X10	00000854		
X11	00051K00		
X12	00000855		
X13	00000S0		Fission spectrum.
X14	00000VC		Velocities.
X15	00000C0		Few-group spacing.
X16	00000NQ		Elements for mixtures.
X17	00000M0		Atom densities.
-----			
X20	00000856		
X21	00C00F0		Flux source.
X22	00000W0		Volumes or radii.
X23	00000857		
X24	40000F2		Flux input.
X25	LX04457		
X26	TRA4001		Return.

X00	8	817	OUTPUT PRINT
X01	TSX4974		
X02	G0000862		
X03	C0C00863		
X04	C0000S1	Fission spectrum.	
X05	C0000V1	Velocity spectrum.	
X06	C0000871		
X07	C0000F2	Fluxes used.	
X10	G0000864		
X11	G0000F4	Output fluxes.	Fl
X12	C0000860		
X13	G0000A0	Input absorptions.	
X14	G0000865		
X15	G0000A2	Output absorption.	
X16	C0000866		
X17	40000Q0	Output sigmas.	
X20	CLA P04	Print velocities	
X21	SUB 404	for each region?	
X22	TNZ X26		
X23	TSX4974	YES	
X24	C0000867		
X25	40000V2		
X26	TSX4973	Punch on line.	
X27	C0000S1		
X30	G0000V1		
X31	40000Q0		
X32	TSX4975		
X33	C0000843		
X34	400020C0		
X35	LXD4457		
X36	IRA4001		

X00	8	822	PLACE ELEMENTS IN REGION BLOCKS
X01	LXA2P02		E → index 2.
X02	10C12X03		E + 1
X03	CLA PQ*		
X04	STA X11		PO block address.
X05	SUB2P2		
X06	STA X12		PO - $h_1 \times G \times E$
X07	CLA2P2		
X10	PAX1		$h_1 \times G \times E$ in index 1 = i.
X11	CLA1000		$\sigma$ element.
X12	STO1000		$\sigma$ region.
X13	20011X11		i - 1 → i
X14	TRA4QC1		Return.

X00	8	823	SET FLUX FOR ELEMENT CALC.
X01	LXD2T10		$r = 1?$
X02	70012X13		If yes, flux supplied, exit.
X03	CLA T11		NO,
X04	STA X11		Set $\varphi_r^g$ address.
X05	AND GC1		
X06	STA X10		$\varphi_{r-1}^g$ address.
X07	LXA1G01		$G \rightarrow g$
X10	CLA1000		Place $\varphi_{r-1}^g \rightarrow \varphi_r^g$
X11	STO1000		
X12	20011X10		$g - 1 \rightarrow g$
X13	TRA4001		$g = 0$ , return.
X14	*	801	

① ↗